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Detailed S-wave velocity structure of sediment and crust off Sanriku, Japan by a new analysis method for distributed acoustic sensing data using a seafloor cable and seismic interferometry

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Abstract

The S-wave velocity (V_s) structure of sediments and the uppermost crust in the landward slope of a subduction zone are important for determining the dynamics of the overriding plate. Although distributed acoustic sensing (DAS) measurements have improved the horizontal resolution of V_s structure in marine areas, the estimations have been limited to the uppermost sedimentary layers. In the present study, we applied seismic interferometry to DAS data of 13 h duration to image the sedimentary and crustal structure offshore of Sanriku, Japan with a spatial horizontal resolution of 2.5 km and > 3.0 km depth. We grouped the DAS data into 10 km long subarrays with 75% overlaps. We first applied a frequency-wavenumber filter to the DAS data to remove DAS instrumental noise and to allow effective extraction of surface waves from short-time records. We then applied a seismic interferometry method and estimated the phase velocities at each subarray. The estimated phase velocities of the fundamental-mode and first higher-mode Rayleigh waves were then used to determine one-dimensional V_s structures for each subarray. The resultant 2-D V_s structure was interpreted as representing sediments and crust. The upper sedimentary layers thicken seaward, while the entire sedimentary unit shows complex lateral variations in depth. The boundary between the sedimentary layers and the uppermost crust varies in depth from 1.8 to 6.8 km and is the deepest in the middle of the profile. Combining this result with the P-wave velocity (V_p) structure along the nearest survey line, determined in previous studies, allowed us to estimate $V_p/V_s = 3.12$, on average, for the lower sedimentary layers. Our method of applying seismic interferometry to marine DAS data broadens the techniques for estimating V_s and V_p/V_s structure of sedimentary layers and the upper crust across subduction zones. These results show that application of the frequency-wavenumber filtering and seismic interferometry to marine DAS data can estimate the V_s structure and the V_p/V_s structure, together with standard marine geophysical surveys of sedimentary layers and the upper crust across subduction zones.

Keywords: S-wave velocity structure, Sediment and upper crust, Distributed acoustic sensing, Seismic interferometry, Seafloor cable, Frequency-wavenumber filter

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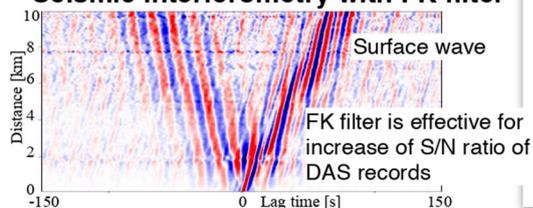
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Graphical Abstract

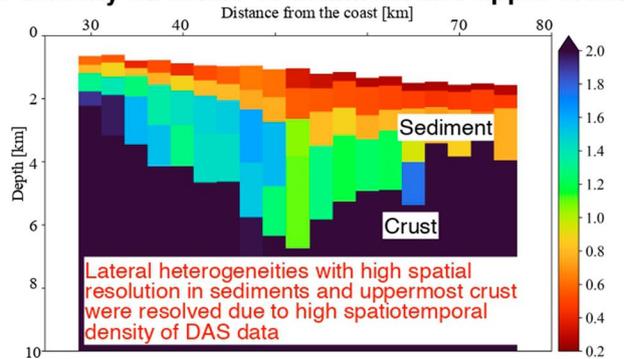
DAS with seafloor cable



Seismic interferometry with FK filter



S-wave velocity structure of sediment and upper crust



Main text

Introduction

Accurate S-wave velocity (V_s) structure of sedimentary layers and the uppermost crust in the landward slope of a subduction zone provide important information about the rheology of the overriding plate. Knowledge of the V_s structures in a shallow part should enhance the accuracy of a wide range of studies, such as hypocenter determination and consideration of rock properties. Since the P-wave velocity (V_p) structures can generally have high resolution, a reliable estimation of the S-wave velocities would provide an accurate estimation of the ratio of P- and S-wave velocities (V_p/V_s), which is useful information for the estimation of rock properties (Ayres and Theilen 1999) and fluid pressure properties (Kodaira et al. 2004).

In the subduction zone of the Japan trench, the recent acquisition of marine multichannel seismic surveys has provided high spatial resolution V_p structures of the sediment and upper crust (Miura et al. 2003; Takahashi et al. 2004). By contrast, the estimation of V_s structures has been limited. Consequently, seismic surveys in the Japan trench could provide estimations of the V_s structures based on the P to S conversion waves observed in data from Ocean Bottom Seismometers (OBSs) (Fujie et al. 2018). Although both seismic interferometry and receiver function methods are useful for estimating V_s with OBS records (Yao et al. 2011; Akuhara et al. 2020; Yamaya et al. 2021), obtaining spatially high-resolution V_s models has been difficult because the distance between OBS locations is typically greater than 6 km along active source seismic profiles and greater than 20 km apart for passive surveys.

In recent years, distributed acoustic sensing (DAS) measurements have been applied to seismic observations (e.g., Zhan 2020). DAS system enables us to measure strain or strain rate with very high spatial resolution over a long distance. The DAS measurement was performed on both the land and seafloor. For example, Dou et al. (2017) estimated shallow shear wave velocity structures by applying the ambient noise method to DAS records on land. In a marine area, Spica et al. (2020) estimated the V_s structure of shallow sediments (to 3 km depth) by applying a frequency–wavenumber (FK) analysis to the seafloor DAS measurements obtained off the Sanriku coast of Japan. However, their estimation of V_s structures was limited to a shallow sediments (< 3.0 km depth). Obtaining the V_s structure throughout the crust is important for deriving the V_p/V_s and the forearc rock properties across subduction zones. The phase velocity of the overtone or long period Rayleigh waves is useful for estimating V_s upper crustal layers, since the phase velocities of these waves are sensitive to V_s .

In the present study, we applied a seismic interferometry method to seafloor DAS records to extract the overtone or long-period (> 5 s) Rayleigh waves. We also proposed a practical method using FK filtering to extract surface waves in the low-frequency range from short-time records with FK filtering. We then estimated the phase velocities from the extracted Rayleigh waves. Finally, we obtained a 2-D V_s structural model of the sedimentary layers and the upper crust for the offshore area of the Sanriku coast of northeastern Japan.

Data and methods

Data

In 1996, the Earthquake Research Institute of the University of Tokyo installed a seafloor seismic tsunami observation system that uses an optical fiber cable in the offshore area of Sanriku (Fig. 1). The length of the buried cable is approximately 120 km, and it extends between 0 and 47.7 km from the coast and covers an area with a sea depth from 0 to 2750 m (Shinohara et al. 2022). The system contains six spare fibers; therefore, DAS measurements have been conducted using a DAS interrogator unit from AP Sensing GmbH (Cedilnik et al. 2019) since 14 February 2019. In the present study, the DAS system recorded strain. The data were recorded at a temporal sampling frequency of 500 Hz, and the duration of the observations in this study was selected to be approximately 13 h. The sensing range, spatial resolution, and gauge length adopted in this study were 100 km, 5.1 m, and 40.79 m, respectively. Shinohara et al. (2019, 2022) and Spica et al. (2020) have described the cable setup and measurement quality of this DAS system.

Calculation of CCFs with an FK filter

Before calculating and stacking the cross-correlation functions (CCFs) of the DAS background noise records, we divided the entire dataset of the DAS array into

10 km-subarrays with a moving window of 75% overlap (Fig. 1). We decimated the original records by first reducing the sampling frequency from 500 to 2 Hz and then stacking 10 adjacent data to enhance the signal-to-noise ratios (SNRs) after filtering the anti-spatial aliasing. The resulting spatial interval of the data was then 51 m.

We computed the CCFs by first dividing continuous records into 10 min time window segments. We allowed for a 50% overlap of each segment to improve SNR. We computed the weighted average of the cross spectra between two channels, following Takagi et al. (2021) and Takeo et al. (2013, 2014). This processing was conducted in the frequency domain. We avoided any earthquake signals by calculating the mean power between 0.025 and 0.2 Hz in the frequency domain for each time window and discarding any data segments whose amplitude exceeded 10 times the amplitude of the previous time window. Takeo et al. (2013) provide more detailed explanations for the calculation of CCFs.

In general, the DAS instrumental noise has a coherent phase at the same time for all stations (Tribaldos and Ajo-Franklin 2021), and this source of noise particularly affects seismic interferometry studies. In the present study, we applied an FK filter to the DAS data to remove this zero-lag noise and to enhance the SNR before calculating and stacking the CCFs. The high spatial density

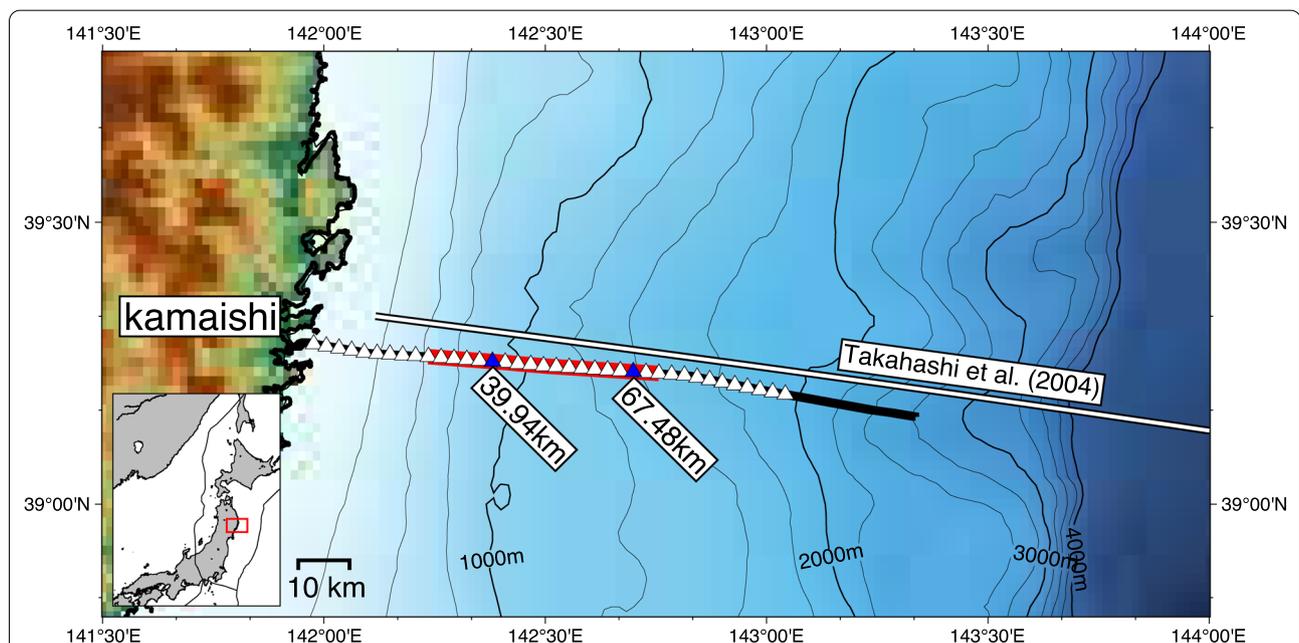


Fig. 1 Location of the seafloor cable containing optical fibers in the off-Sanriku region, Japan. Location of the optical seafloor cable in the off-Sanriku region, Japan. The black line indicates the route of the seafloor cable installed by the Earthquake Research Institute, the University of Tokyo. White triangles indicate the centers of the subarrays for calculation of the CCFs. Blue triangles indicate the centers at the distances from the coast of 39.94 and 67.48 km for the data processing demonstrated in Fig. 2 and 3. The red line shows a span of the estimated 2-D velocity profile shown in Fig. 4. Due to large incoherent noise near the coast and offshore areas, the spatial range of the present data processing was limited from 28 to 75 km from the coast. White lines indicate the survey lines of Takahashi et al. (2004)

of the DAS data enables the application of spatial Fourier transform; therefore, we performed a 2-D Fourier transform in the FK domain (Hudson et al. 2021; Atterholt et al. 2022). The zero-lag noise, which has an infinite phase velocity, is mapped to the zero wavenumber in the FK domain. We designed an FK filter $w(f, k)$ as:

$$w(f, k) = g(f, k, c_{\min}) * (1 - s(f, k, c_{\max})), \quad (1)$$

where $g(f, k, c_{\min})$ is a 10% Tukey window used to eliminate signals slower than the cut-off minimum phase velocity c_{\min} . $g(f, k, c_{\min})$ is defined as:

$$g(k, f, c_{\min}) = \begin{cases} 1, & \text{for } -0.4k_{\max} < k < 0.4k_{\max} \\ 0, & \text{for } k < -0.5k_{\max} \text{ or } k > 0.5k_{\max} \\ \frac{1}{2} \left[1 + \cos \left\{ \pi \left(1 - \frac{k}{0.1k_{\max}} \right) \right\} \right], & \text{otherwise} \end{cases}, \quad (2)$$

where $k_{\max} = 4\pi f / c_{\min}$. Furthermore, $s(f, k, c_{\max})$ is an 8-th order Kaiser filter that removes the signal faster than the maximum phase velocity c_{\max} , including the zero-lag noise. In this study, we enhanced the surface wave signals by setting c_{\min} and c_{\max} to 0.35 km/s and 4.00 km/s, respectively.

Phase velocity estimation

In this section (Phase velocity estimation), we obtained the phase-velocity dispersion curves for the Rayleigh waves using the CCFs of the ambient noises recorded by the DAS observation. At the same time, we determined the 1-D V_s structures and errors of the phase velocities. In the next section (Inversion of the S-wave velocity structure), we provide more accurate estimates of the 1-D V_s structures using only the reliable frequency range of the dispersion curves (i.e., those with small errors) obtained in this section.

We adopted the spatial auto-correlation (SPAC) method to estimate the phase velocity (Aki 1957; Okada 2006; Nishida et al. 2008b), because the SPAC method represents the observed cross-spectra assuming a laterally homogeneous structure and a homogenous source distribution. According to Nakahara et al. (2021), the synthetic cross-spectrum for radial strain records (e.g., DAS) is defined as:

$$S_{ij}^{\text{syn.}}(\omega, c_R, c_L) = A_R(\omega) \left[3J_0\left(\frac{\omega}{c_R} d_{ij}\right) - 4J_2\left(\frac{\omega}{c_R} d_{ij}\right) + J_4\left(\frac{\omega}{c_R} d_{ij}\right) \right] + B_L(\omega) \left[J_0\left(\frac{\omega}{c_L} d_{ij}\right) - J_4\left(\frac{\omega}{c_L} d_{ij}\right) \right], \quad (3)$$

where ω is the angular frequency, A_R is the power spectrum for the Rayleigh wave, B_L is the power spectrum for the Love wave, J_n is the n th-order Bessel function of the first kind, d_{ij} is the distance between i th and j th

channels, c_R is the phase velocity of the Rayleigh wave, and c_L is the phase velocity of the Love wave. In Eq. 3, the first and second terms represent the Rayleigh and Love waves, respectively. In general, the Love waves have less energy than the Rayleigh waves at a period range below 0.1 Hz (Nishida et al. 2008a). Furthermore, as mentioned by Nakahara et al. (2021), Rayleigh waves predominate in the far field. The envelope of the Rayleigh wave term decays with an order of $d^{-1/2}$, while the Love wave term decays with an order of $d^{-3/2}$ in the far field. For these reasons, and given the small estimated contribution of the Love wave terms, we obtained our misfit function E as:

$$L2(\omega, c_R) = \sum_{ij} \left(\text{Re} \left[S_{ij}^{\text{obs}}(\omega) \right] - S_{ij}^{\text{syn.}}(\omega, c_R) \right)^2, \quad (4)$$

$$E(\beta_l, h_l) = \frac{1}{\omega} \int L2(\omega, c_R(\omega; \beta_l; h_l)) d\omega, \quad (5)$$

where $S_{ij}^{\text{obs}}(\omega)$ and $S_{ij}^{\text{syn.}}(\omega)$ are the observed and synthetic cross-spectra between i th and j th channels calculated from Eq. 3, respectively. β_l and h_l are the V_s and thickness at the l th layer, respectively. We followed the methods described by Takeo et al. (2022) and Yoshizawa & Kennett (2002) to estimate the phase velocity model. β_l and h_l are model parameters for minimizing $E(\beta_l, h_l)$ in Eq. 5. In this study, we adopted the simulated annealing algorithm of Goffe et al. (1994) as a global optimizer in our search for model parameters. We avoided numerical instability by constraining the V_s at each layer at greater than 80% of the value of the layer directly above it.

In practice, we estimated the phase velocity and evaluated the errors in the estimated phase velocity. First, we estimated the dispersion curves of the phase velocity from the cross-spectra for all pairs of channels for each subarray. We then obtained a 1-D model with six layers, where the deepest layer had an infinite thickness for each subarray. We adopted the scaling relationship between V_p , V_s , and density described by Brocher (2005). Next, searching by trial and error, we divided the subarrays into two groups according to the distances from the coast and frequency range. The dispersion curves of the phase velocity were estimated using the only fundamental mode of the Rayleigh wave at the frequency range

between 0.08 and 0.50 Hz for one group that had distances ranging from 28 to 52 km from the coast. For the other group with distances ranging from 52 to 75 km, the fundamental mode (0.08–0.50 Hz) and the first higher

mode (0.25–0.50 Hz or 0.08–0.50 Hz) of Rayleigh wave were used to obtain a dispersion curve. Due to large incoherent noise near the coast and offshore areas, the spatial range of the present data processing was limited from 28 to 75 km from the coast. Synthetic phase velocities were calculated using DISPER80 (Saito 1988).

We also used the bootstrap method (Efron 1992) to estimate errors. We aggregated station pairs randomly selected from all station pairs, allowing for overlap for a bootstrap sample. We then calculated the standard deviation of 100 dispersion curves estimated from each of the 100 bootstrap samples. The V_s structures estimated from the data of all pairs of channels for each subarray were used as the reference model.

Inversion of the S-wave velocity structure

The phase velocity of the Rayleigh wave estimated by seismic interferometry was used to obtain a 1-D V_s isotropic model. The 1-D V_s structure was determined by minimizing the misfit function E , as defined by:

$$E = \sqrt{\frac{1}{N} \sum \left[\frac{c_{obs}(\omega) - c_{syn}(\omega; \beta_l; h_l)}{c_{err}(\omega)} \right]^2}, \quad (6)$$

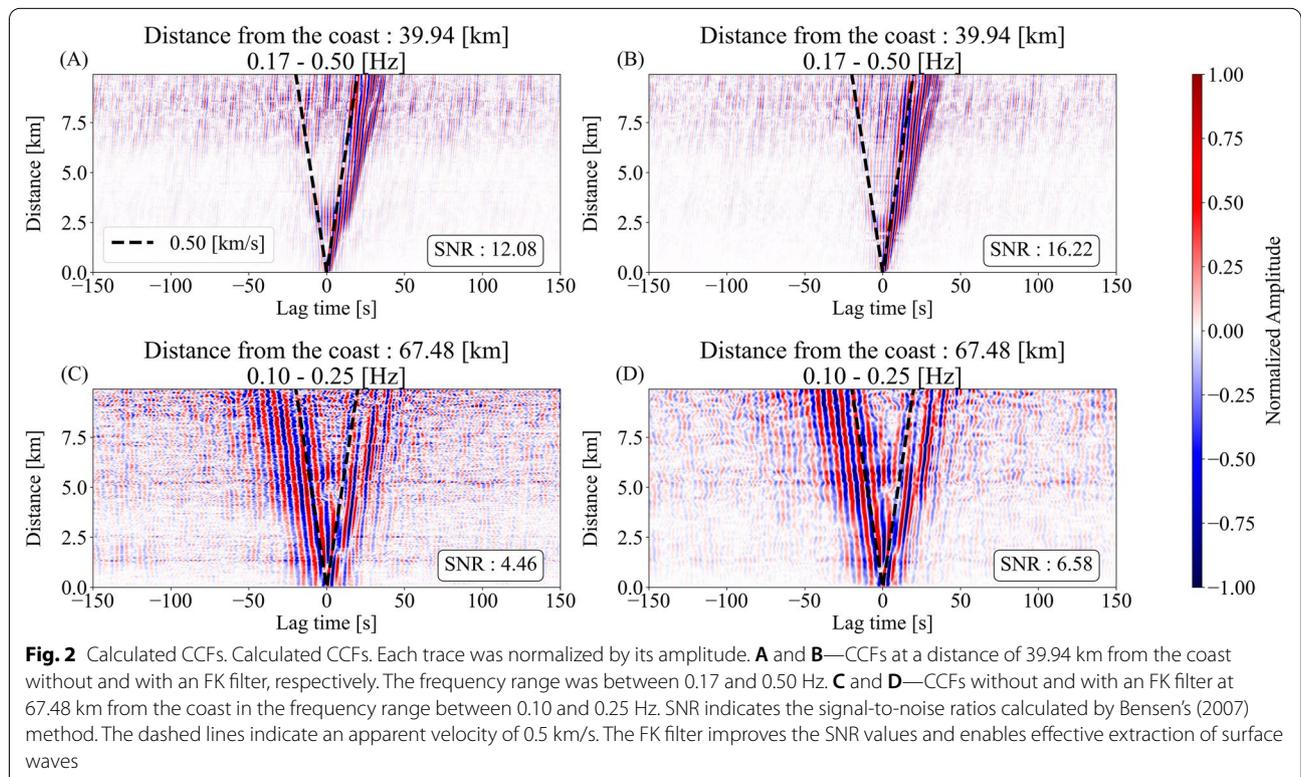
where N is the number of estimated phase velocities, and c_{obs} , c_{syn} and c_{err} indicate the observed, synthesized, and uncertainty of the phase velocity, respectively. We obtained a stable result by selecting only a frequency

band with phase velocities with an error lower than 0.1 km/s for the inversion analysis. We again set the V_s (β_l) and thickness (h_l) as the model parameters to minimize the value obtained from Eq. 6. We then used the simulated annealing algorithm method to obtain the optimal model parameters. The bootstrap average models estimated from the phase velocity estimation were used as the reference model. We estimated errors using the bootstrap method once again. Here, we aggregated a final dispersion curve randomly selected from the 100 dispersion curves estimated in the previous section (Takeo et al. 2013).

The 1-D V_s structures were estimated on the assumption that we could ignore the effect of lateral heterogeneity for profiles perpendicular to the seafloor cable. Previous seismic reflection and refraction surveys support this assumption since profiles perpendicular to the seafloor cable show little lateral heterogeneity to a depth of 10 km (e. g. Takahashi et al. 2004).

Results and discussion

We computed the CCFs between all possible pairs of each subarray, and the resulting CCFs clearly showed a surface wave (Fig. 2). The group velocities of about 0.5 km/s were much slower than the surface waves from land observations in the same period range. The surface wave with low velocity corresponded to a special type of



Rayleigh wave or Scholte wave (Stokoe et al. 1991; Bagheri et al. 2015) because the Love wave had less energy than the Rayleigh wave in the period range below 0.1 Hz. The SNR was much higher for the CCFs with the FK filter than without the FK filter. We used the method of Bensen et al. (2007) to estimate the SNR.

We selected the dispersion curve using the CCFs (Figs. 3-A and 3-E). Extracting the Rayleigh waves by interferometry enabled a stable estimation of the dispersion curves with errors less than 0.1 km/s by bootstrapping. Near the coast (Fig. 3A), the fundamental Rayleigh wave was dominant in the frequency range between 0.2 and 0.5 Hz. By contrast, in the case of an offshore subarray (Fig. 3E), both the fundamental (0.5–0.1 Hz) and the 1st higher mode (0.5–0.2 Hz) Rayleigh waves predominated. This result clearly indicates that the thickness of the low- V_s layer differs between the near-coast and offshore areas. We determined the V_s structure using only the phase velocities of the fundamental mode of Rayleigh waves in the near-coast area at distances between 28 and 52 km. In the area where the distance was greater than 52 km from the coast, both the fundamental and first higher modes of the Rayleigh waves were used for phase velocity estimation.

We inverted the measured phase velocities into 1-D V_s structures (Fig. 3) below each subarray and calculated the 1-D V_s structures (Fig. 3B and F) and normalized V_s sensitivity kernels (Fig. 3C, G, and I) of the Rayleigh waves. Errors were calculated using the bootstrap method. A small error was estimated in the depth range where V_s values were slower than 2.0 km/s. The synthetic phase velocities calculated by DISPER80 using the 1-D V_s inversion results were consistent with the observations (Figs. 3D and H). Given that the sensitivity kernel had high sensitivity in the depth range of V_s slower than 2.0 km/s, our inversion provided a V_s structure with small errors at that depth range of V_s . By contrast, the layers of V_s greater than 2.0 km/s were not estimated well. However, the V_s sharply increases to those greater than 2.0 km/s at the boundary between the shallow slow layers and the layers below, and the mutual velocity ranges, with errors, are clearly separated. Therefore, the depth was reliably estimated for the discontinuity between the shallow slow layers and the layers below.

Finally, a 2-D V_s profile (Fig. 4) was obtained from the 1-D V_s structures at each subarray. Although each 1-D V_s structure at a given subarray was composed of six layers, we classified this 2-D profile into four units with a clear velocity discontinuity (Fig. 4). The velocities of some contiguous layers were coincident in terms of errors. In those cases, we unified the contiguous layers into one unit. The V_s of Unit-1 at depths of 0.7–2.6 km and Unit-2 at the depth of 0.9–4.0 km were slower than

0.6 km/s and approximately 0.7 km/s, respectively. The V_s of Unit-3 at depths of 1.2–6.8 km and Unit-4 layers below the Unit-3 were 1.1–1.8 km/s and greater than 2.0 km/s, respectively.

We compared our 2-D V_s structure (Fig. 4) with the V_s and V_p structures obtained in other studies to interpret these units. The V_s values of Unit-1 and Unit-2 layers, at less than 0.6 km/s and about 0.7 km/s, respectively, were consistent with the results presented by Spica et al. (2020) with the same profile. Takahashi et al. (2004) provided the V_p structure estimated by refraction surveys along a profile parallel to our DAS cable, positioned northward, with a distance of about 20 km from the seafloor cable (Fig. 1). The V_p values of Unit-1 and Unit-2 in the present study were determined as 1.7 and 2.3 km/s, respectively, and these layers were interpreted as Neogene sediment by Spica et al. (2020). The thicknesses of both Unit-1 and Unit-2 increased seaward for a distance range from 28 to 47 km. This increase in thickness is also consistent with the results reported by previous studies. In distance range further from the coast between 47 and 75 km, however, the thicknesses of Unit-1 and Unit-2 showed very small variations.

The thickness of Unit-3 was 0.6 km at a distance of 28 km from the coast and increased with a horizontal distance. Unit-3 became the thickest (4.1 km) at a distance from 52 km from the coast. The thickness of Unit-3 decreased to 1.9 km at a distance of 65 km. At distances between 65 and 75 km, Unit-3 appeared to pinch out. These strong lateral heterogeneities in Unit-3 were also evident in the V_p model by Takahashi et al. (2004). The discontinuity observed between Unit-3 and Unit-4 can be interpreted as the boundary between sediments and the island arc uppermost crust consistent with the interpretation reported by Takahashi et al. (2004). Along the same Japan trench offshore Ibaraki and the south of the study area, Yamaya et al. (2021) obtained V_s values of the deepest sediment of approximately 2.1 km/s using records from pop-up ocean bottom seismometers. In contrast, Unit-3 in this study has smaller V_s compared to the results off Ibaraki. We attribute the difference in V_s values for the two regions to differences in porosities and lithologies in the lowermost sedimentary layers.

Although our V_s profile and the V_p profile of Takahashi et al. (2004) are 20 km apart (Fig. 1) and the spatial resolution of our results is much higher than that of Takahashi et al. (2004), we calculated the average value and errors of the V_p/V_s (Fig. 4) using the V_p estimated by Takahashi et al. (2004) to support our interpretation of the results. The errors were defined as twice the standard deviation during calculation of the average. The average V_p/V_s values of Unit-1 and Unit-2 were 5.00 and 3.34, respectively. The V_s in Unit-3 of 1.1–1.8 km/s

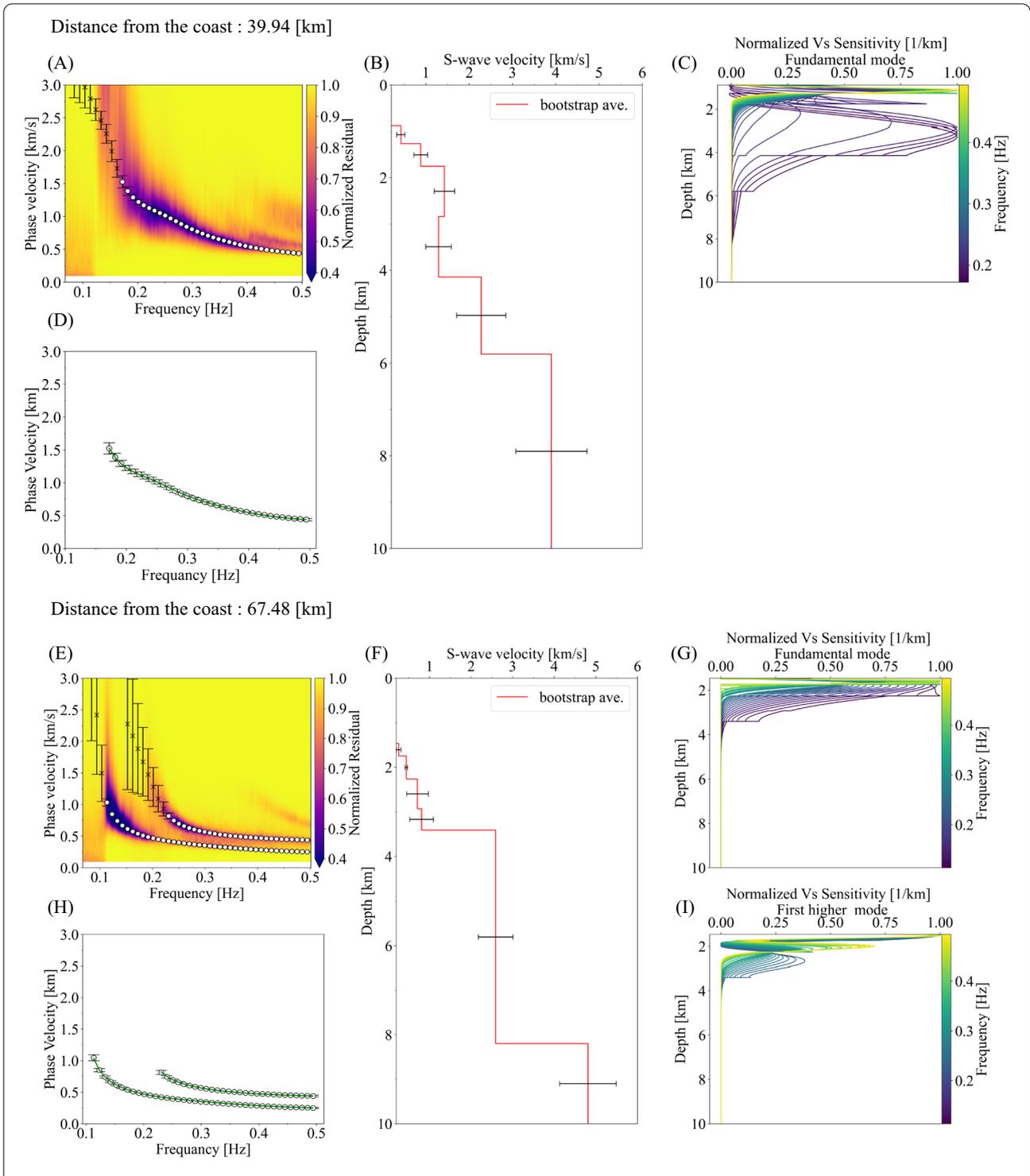
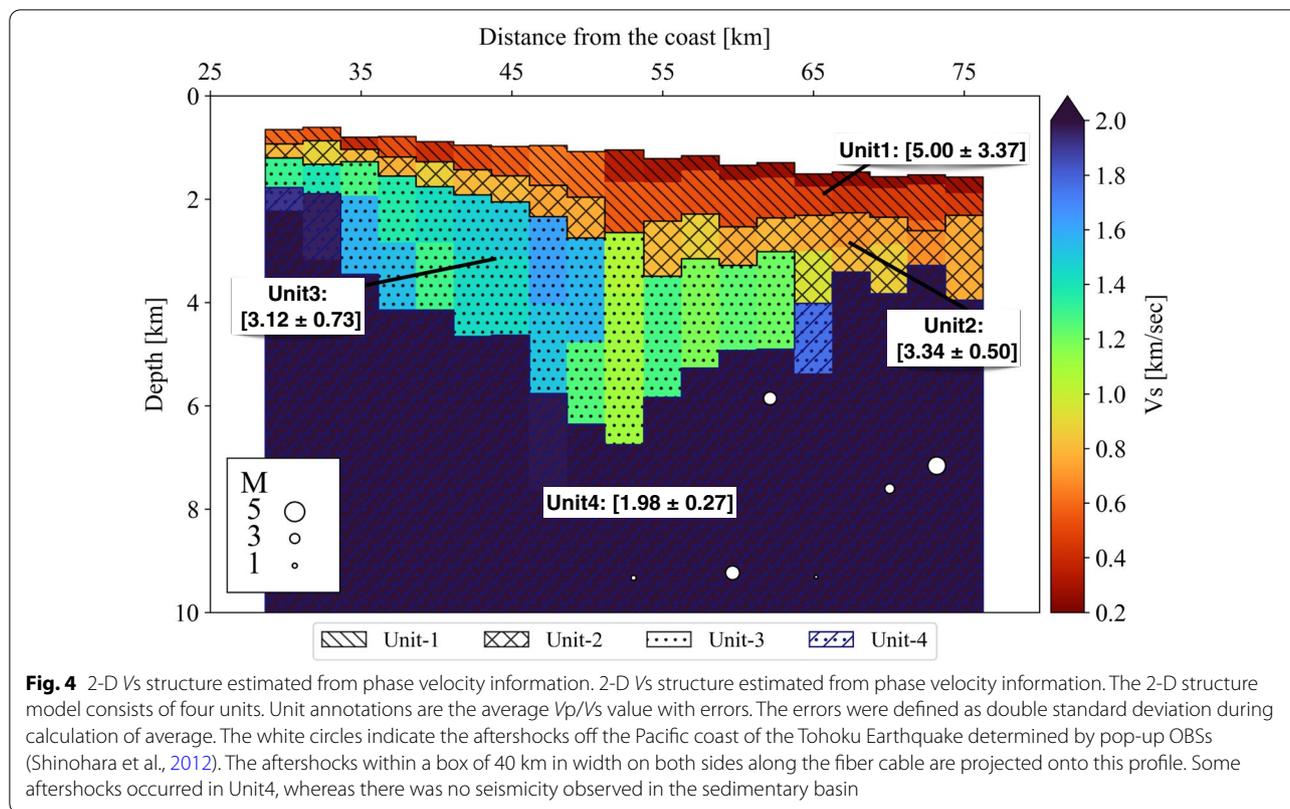


Fig. 3 Phase velocity, V_s structures, and sensitivity kernel. **A** and **E**—Normalize residuals and estimation phase velocity at subarrays from the coast of 39.94 and 67.68 km, respectively. The error bars represent the uncertainties estimated by the bootstrap method. The white dots and cross makers indicate errors less than and more than 0.1 km/s, respectively. We used phase velocity only with an error less than 0.1 km/s for our inversion analysis. **B** and **F**— V_s structures at subarrays from the coast of 39.94 and 67.68 km. **D** and **H** White dots and green lines indicate the observed and estimated phase velocities, respectively. The errors were estimated by the bootstrap method. **C** Normalized V_s sensitivity kernel of the fundamental Rayleigh wave at 39.94 km from the coast. **G** and **I** Normalized V_s sensitivity kernels of fundamental and first higher mode Rayleigh waves at 67.68 km from the coast



was obtained from this study and the V_p in Unit-3 was estimated to be 4.2 km/s by Takahashi et al. (2004). As a result, the average V_p/V_s value in Unit-3 become 3.12. On the other hand, the V_p/V_s of Unit-4 was 1.98 from a V_s of > 2.0 km/s and a V_p of 5.0 km/s.

Because we found no previous reports on the V_p/V_s of marine sedimentary layers in our study area, we compared V_p/V_s with the values obtained in other marine areas for the similar geological ages. V_p/V_s values of sedimentary layers are known to vary depending on porosity of rocks, constitutive materials, and tectonic settings from place to place (e.g., Kodaira et al. 1996). We chose the ages of sediments as an indicator of the comparison rather than the mineral components, because porosity of medium primarily affects V_s of sediments and uppermost crust under marine environment. A comparison of the thickness of each Unit in our results to those of the layers obtained by Takahashi et al. (2004) indicates that Unit-1 and Unit-2 are Neogene sediments, and Unit-3 is Cretaceous sediments. The V_p/V_s of the layer deposited in Neogene was estimated at 5.10 in Norway (Kvarven et al. 2015) and 3.2–4.4 in the landward slope on the southern Japan trench (Yamaya et al. 2021). These values are comparable to our estimation of V_p/V_s in Unit-1 and Unit-2. Kodaira et al. (1996) reported that the V_p/V_s of

the sedimentary layers in Norway ranged from 5 to 3, although their ages were unknown. By contrast, Kvarven et al. (2015) reported a V_p/V_s of 1.78 for the Cretaceous sediment layer in Norway. On the other hand, Yamaya et al. (2021) showed a V_p/V_s of 2.1 for the Cretaceous sediment layer beneath the landward slope of the southern Japan trench. Although our V_p/V_s values are believed to have some uncertainty due to lower spatial resolution of V_p results from the airgun-OBS surveys, the V_p/V_s for the Cretaceous sediment unit in our study region can be concluded to have large value obviously from a point of view of the errors estimated in this study. We therefore infer that the Cretaceous sediments in this study area is unconsolidated.

Now let us consider our result on a deep part or the crust. Using stationary seismic networks in land and sea by body-wave travel-time tomography, Matsubara et al. (2019) reported V_p/V_s of 1.6–1.9 for the upper crust below the northeastern Japan island arc. In our study, the V_p/V_s for Unit-4 seems to correspond to the uppermost part of the island arc crust from the point of view of their V_p/V_s . Furthermore, aftershocks of the 2011 Tohoku-oki earthquake, as estimated by Shinohara et al. (2012), were located only in Unit-4 (Fig. 4), whereas no seismicity was experienced in the other three units. In summary, Unit-1,

Unit-2, and Unit-3 consist of sedimentary layers, whereas Unit-4 represents the uppermost part of the igneous crust of an island arc.

Previous studies that estimated V_s structures using DAS records have been limited to elucidation of a shallow part of the sediment layers. For example, Spica et al. (2020) estimated the V_s structure to 3 km in depth. The application of the seismic interferometry with FK filtering to the DAS data now enabled the determination of phase velocities of surface waves whose periods are longer than those of previous studies. Using DAS data with high spatial resolution we were able to obtain an S-wave structure of lowermost sediment > 3.0 km depth and extending to 6.8 km depth where sediments were thickest.

The SPAC method is useful to estimate velocity structure using data from a seismic network; however, spatial aliasing due to a sparse distribution of stations causes uncertainty for the SPAC analysis. Because DAS measurement has a high-spatial density, spatial aliasing can be avoided. For example, we could prevent misidentification of a mode branch. V_s structures in marine area have conventionally been estimated by the observation of converted waves during seismic surveys or by seismic interferometry using spatially dense OBSs data. Our method offers a new approach for determining the V_s of shallow structures with high spatial resolution in marine areas using short-term DAS data and a seafloor cable. A shallow V_s structure in a marine area with high resolution by our method leads to a detailed distribution of V_p/V_s in a shallow region, which is useful for considering tectonics and rock properties.

Conclusions

The information of V_s is important for understanding the rock properties of the upper crust and sediments on the seafloor. We applied a seismic interferometry method to DAS records obtained during a recording period of 13 h by a seafloor cable installed off Sanriku, Japan. We found that applying the FK filter to the DAS data before calculating the CCFs effectively enhances the surface waves. The phase velocities of the Rayleigh waves were calculated by the SPAC method. Finally, we inverted the V_s structure from the phase velocities of the Rayleigh waves obtained from seismic interferometry. The V_s structures of the sediment layers and the upper crust were consistent with those determined by refraction surveys. The seismic interferometry method with DAS data collected through seafloor cables could estimate V_s structures with high spatial resolution.

The V_s structure of sediment layers has been widely explored using seismic interferometry and receiver function methods with OBS data. However, their spatial

resolution is constrained by the spatial density of the installed OBSs. By contrast, a V_s structure with high spatial resolution can be estimated from short-term DAS records by applying the seismic interferometry method. Our results identified a new approach for estimating the heterogeneous V_s structure of sediment layers and the upper crust in subduction zones.

Abbreviations

V_s : S-wave velocity; V_p : P-wave velocity; V_p/V_s : Ratio of P- and S-wave velocities; DAS: Distributed acoustic sensing; FK: Frequency–wavenumber; CCFs: Cross-correlation functions; SNRs: Signal-to-noise ratios; SPAC: Spatial auto-correlation; OBSs: Ocean bottom seismometers.

Supplementary Information

The online version contains supplementary material available at <https://doi.org/10.1186/s40623-022-01652-z>.

Additional file 1: Figure S1. Effectiveness of frequency-wave number (FK) filter for calculation of CCFs. The CCFs with FK filter ((B), (D) and (F)) are compared those without FK filter ((A), (C) and (E)). The CCFs at distances of 39.94 km, 54.95 km, and 64.97 km are shown in pairs of (A) and (B), (C) and (D), and (E) and (F), respectively. Each trace was filtered from 0.1 Hz to 0.2 Hz and was normalized by its amplitude. Seismic signals propagating with an apparent velocity range from 0.35 km/s to 4.0 km/s were selected by FK filtering. For the estimation of signal-to-noise ratio calculated by root mean square amplitude ratio between surface wave and noise data for the last 50s, the method of Bensen et al. (2007) was used. DAS instrument generally has a coherent noise has at the same timing in all stations (zero-lag noise) and the coherent noise interfere analyses for surfaces waves. We can remove the zero-lag noise by using FK filter due to difference of apparent velocity. Applying FK filter to DAS data before calculating CCFs effectively enhances surface waves in DAS records. **Figure S2.** Calculated cross correlation functions (CCFs) with a frequency-wave number filter at the frequency range between 0.08 and 0.50 Hz. Each trace was normalized by its amplitude. (A), (B), and (C) denote CCFs at distances of 29.93, 32.43, and 64.97 km from the coast, respectively. The dashed lines indicate an apparent velocity of 0.5 km/s. Note that the seismic waves propagating with velocities of approximately 0.5 km/s are recognized in the CCFs. The group velocities of about 0.5 km/s were much slower than the surface waves in land for an identical period range. The surface wave propagating with a low velocity is estimated to correspond to a special type of Rayleigh wave or Scholte wave. **Figure S3:** Normalized residuals and estimation of phase velocities in the subarrays from the coast of 29.93 (A), 32.43 (B), and 64.97 (C). Bars indicate phase-velocity uncertainties, which were estimated by a bootstrap method. The estimated phase velocities with errors less than 0.1 km/s are indicated by white circles. Although the fundamental Rayleigh wave was dominant near the coast, both fundamental (0.5–0.1 Hz) and 1st higher mode (0.5–0.2 Hz) Rayleigh waves appeared far from the coast. The faster phase velocities were observed in areas closer to the coast. **Figure S4.** The obtained V_s structures at subarrays centered at distances at 29.93 km (A), 32.43 km (B), and 64.97 km (C) from the coast. The errors were estimated by the bootstrap method. V_s and thickness in each layer are set to be model parameters and minimized values of the misfit function between observed and synthetic dispersion curves in Equation 6

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Author contributions

SF played a leading role in this study, including data processing, analysis, and completion of the manuscript. MS and TY led the temporal DAS observation and interpreted the results. KN, AT, and KY contributed to develop the analysis method and interpreted the results. All authors read and approved the final manuscript.

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Availability of data and materials

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Declarations**Ethics approval and consent to participate**

Not applicable.

Consent for publication

Not applicable.

Competing interests

The authors declare that they have no competing interest.

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